

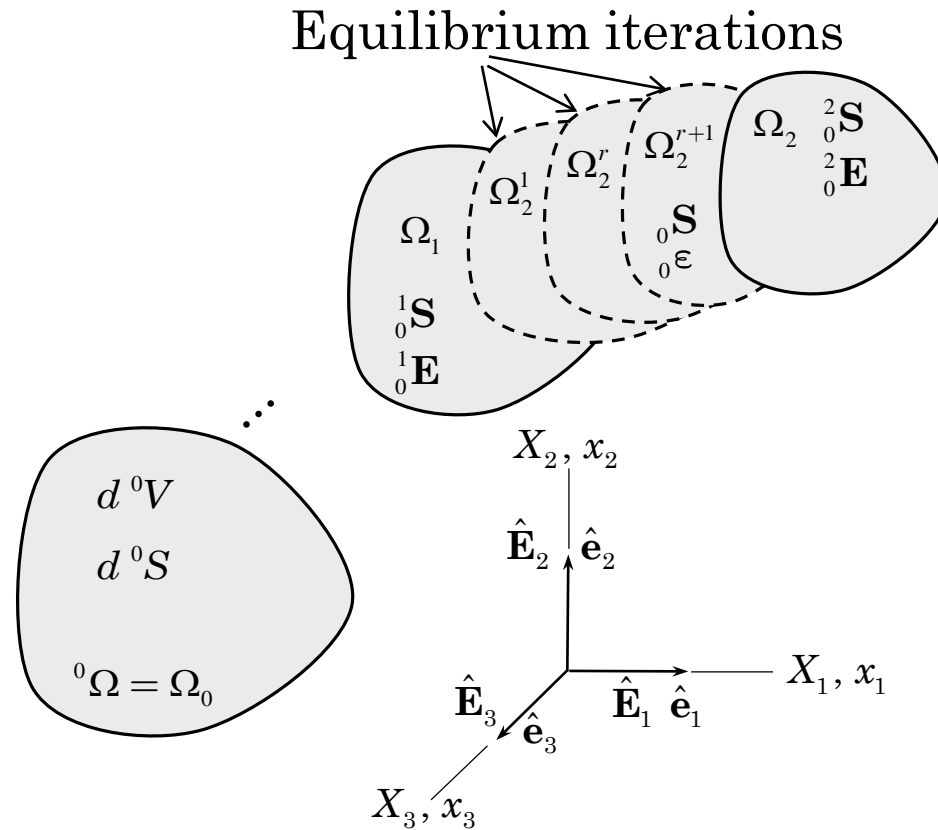


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# **CONTINUUM SHELL ELEMENT AND POSTBUCKLING ANALYSIS**

- **Description of continuum shell element  
(principle of virtual displacements)**
- **Post-buckling analysis of composite panels and  
comparison with experimental results**

# CONTINUUM SHELL ELEMENT



# CONTINUUM SHELL ELEMENT

Principle of virtual displacement applied to the configuration to be determined

$$\int_{t+\Delta t V} {}^{t+\Delta t}\sigma_{ij} \delta {}_{t+\Delta t}e_{ij} {}^{t+\Delta t}dV = {}^{t+\Delta t}R$$

Use energy conjugacy to write all integrals on the reference configuration

$$\int_{t+\Delta t V} {}^{t+\Delta t}t_{ij} \delta({}_{t+\Delta t}e_{ij}) {}^{t+\Delta t}dV = \int_{{}_0V} {}_0^{t+\Delta t}S_{ij} \delta({}_0^{t+\Delta t}\varepsilon_{ij}) {}_0dV$$

$$\int_{{}_0V} {}_0^{t+\Delta t}S_{ij} \delta({}_0^{t+\Delta t}\varepsilon_{ij}) {}_0dV = {}^{t+\Delta t}R$$

$${}^{t+\Delta t}R = \int_{{}_0A} {}_0^{t+\Delta t}t_k \delta u_k {}_0dA + \int_{{}_0V} {}_0\rho {}_0^{t+\Delta t}f_k \delta u_k {}_0dV$$

# CONTINUUM SHELL ELEMENT

## Decompositions

$$\begin{aligned} {}_0^{t+\Delta t} S_{ij} &= {}_0^t S_{ij} + {}_0 S_{ij} & {}_0 \varepsilon_{ij} &= {}_0 \ell_{ij} + {}_0 \eta_{ij} \\ {}_0^{t+\Delta t} \varepsilon_{ij} &= {}_0^t \varepsilon_{ij} + {}_0 \varepsilon_{ij} & {}_0 \eta_{ij} &= \frac{1}{2} ({}_0 u_{k,i} {}_0 u_{k,j} \\ {}_0 \ell_{ij} &= \frac{1}{2} ({}_0 u_{i,j} + {}_0 u_{j,i} + {}_0^t u_{k,i} {}_0 u_{k,j} + {}_0 u_{k,i} {}_0^t u_{k,j}) \end{aligned}$$

$$\delta({}_0^{t+\Delta t} \varepsilon_{ij}) = \delta({}_0^t \varepsilon_{ij}) + \delta({}_0 \varepsilon_{ij}) = \delta({}_0 \varepsilon_{ij})$$

$${}_0 S_{ij} = {}_0 C_{ijrs} {}_0 \varepsilon_{rs}, \quad {}_0 S_{ij} = {}_0 C_{ijrs} {}_0 \ell_{rs}$$

## Final virtual work statement

$$\begin{aligned} &\int_{{}_0 V} {}_0 C_{ijrs} {}_0 \ell_{rs} \delta({}_0 \varepsilon_{ij}) {}_0 dV + \int_{{}_0 V} {}_0^t S_{ij} \delta({}_0 \eta_{ij}) {}_0 dV \\ &= {}_0^{t+\Delta t} R - \int_{{}_0 V} {}_0^t S_{ij} \delta({}_0 \ell_{ij}) {}_0 dV \end{aligned}$$

# CONTINUUM SHELL ELEMENT

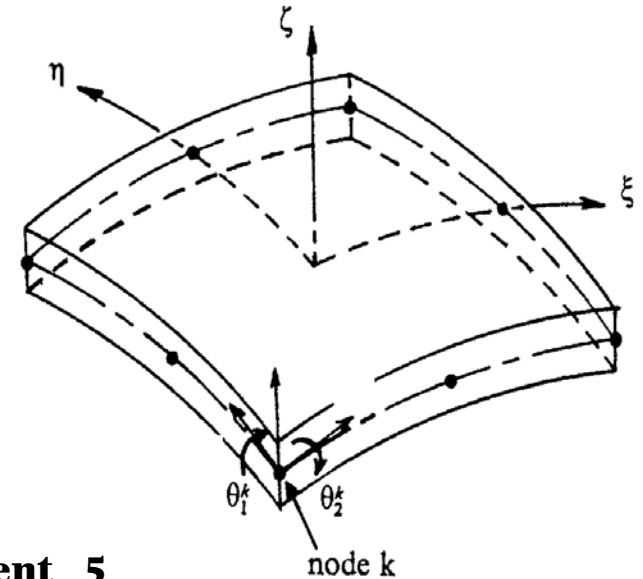
(continued)

## Assumed Kinematics of the Shell Element

$${}^t x_i = \sum_{k=1}^n \psi_k(\xi, \eta) [{}^t x_i^k + \frac{\zeta}{2} h_k {}^t e_{3i}^k]$$

$${}^t u_i = {}^t x_i - {}^0 x_1 = \sum_{k=1}^n \psi_k(\xi, \eta) [{}^t u_k^k + \frac{\zeta}{2} h_k ({}^t e_{3i}^k - {}^0 e_{3i}^k)]$$

$$u_i = {}^{t+\Delta t} u_i - {}^t u_i = \sum_{k=1}^n \psi_k(\xi, \eta) [u_i^k + \frac{\zeta}{2} h_k ({}^{t+\Delta t} e_{3i}^k - {}^t e_{3i}^k)]$$



# A NUMERICAL EXAMPLE

Symmetry line:

$$u_1 = \phi_1 = 0$$

Simply supported:

$$u_1 = u_2 = u_3 = \phi_2 = 0$$

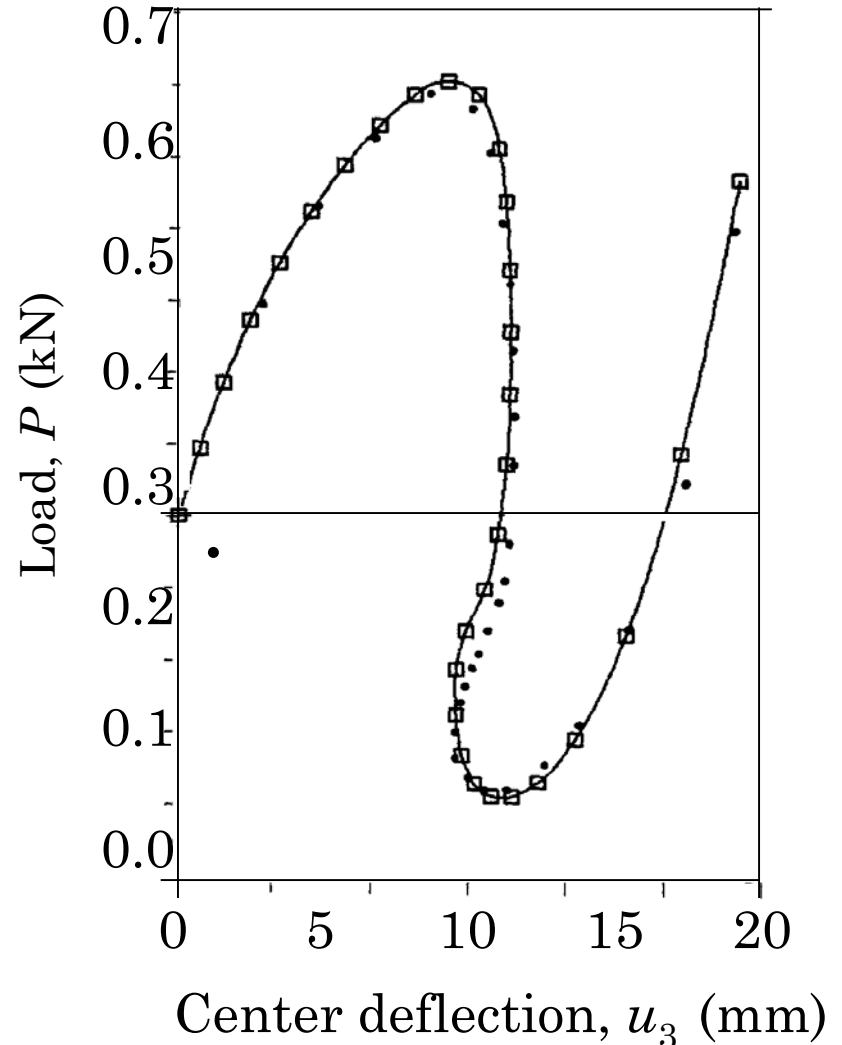
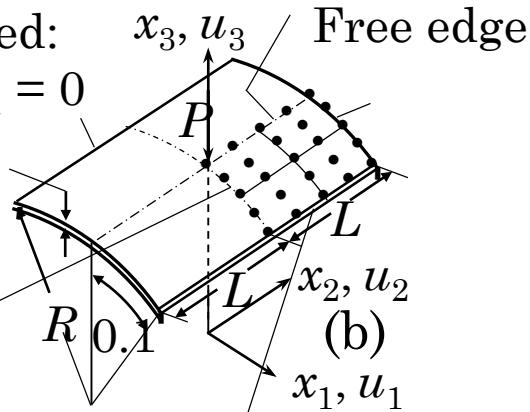
$$h = 6.35 \text{ mm}$$

Symmetry line:

$$u_2 = \phi_2 = 0$$

Simply supported:

$$u_1 = u_2 = u_3 = \phi_2 = 0$$



$$E = 3103 \text{ N/mm}^2, \nu = 0.3$$

$$R = 2540 \text{ mm}, L = 254 \text{ mm}$$

# POSTBUCKLING AND FAILURE ANALYSIS - AN EXAMPLE

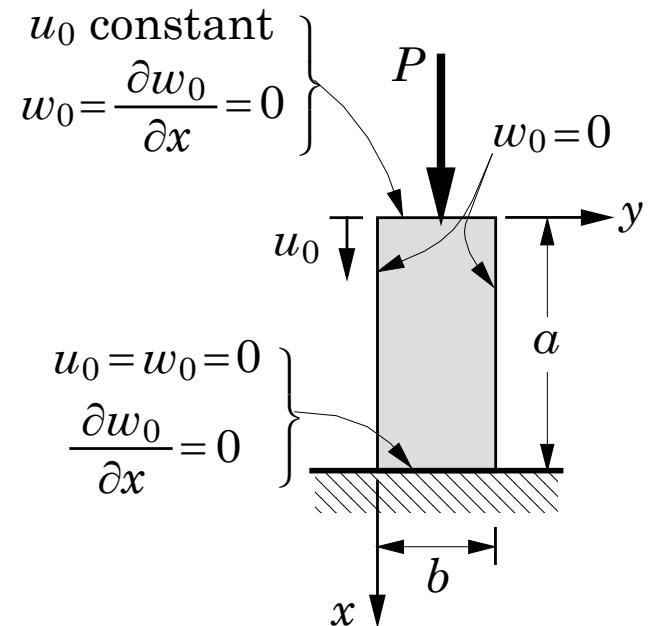
- Nonlinear FE analysis
- Comparison with experimental results of Starnes and Rouse
- Progressive failure analysis

$a = 50.8 \text{ cm (20 in.)}$ ,  $b = 17.8 \text{ cm (7 in.)}$ ,  
 $h_k = 0.14 \text{ mm (0.0055 in.)}$

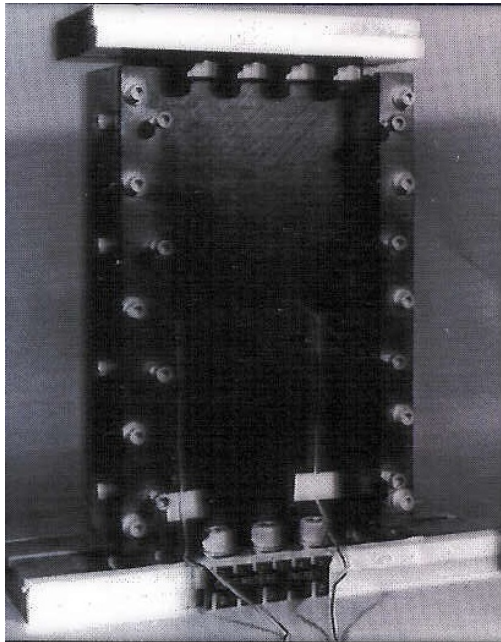
24-ply laminate:  $[45/-45/0_2/45/-45/0_2/45/-45/0/90]_s$

$E_1 = 131 \text{ Gpa (19,000 ksi)}$ ,  $E_2 = 13 \text{ Gpa (1,890 ksi)}$ ,

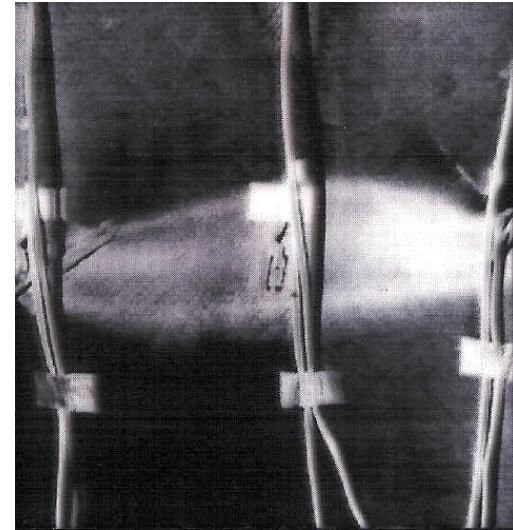
$G_{12} = 6.4 \text{ Gpa (930 ksi)}$ ,  $\nu_{12} = 0.38$   
 (graphite-epoxy)



# Experimental Setup and Failure Region (Starnes & Rouse, NASA Langley)



(a) Typical panel  
with test fixture



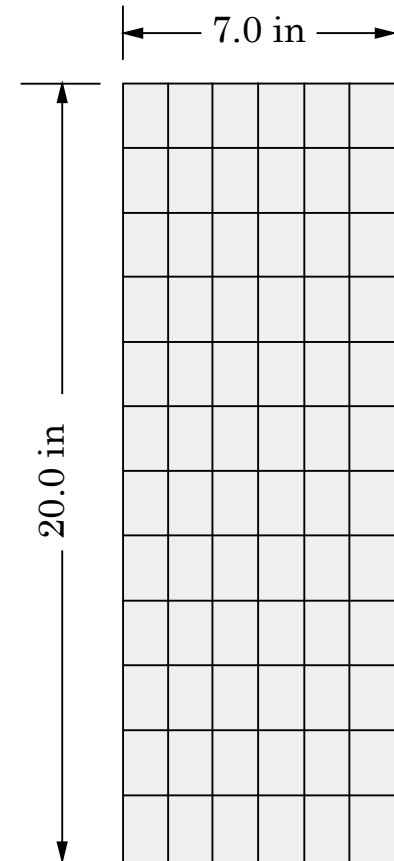
(b) A transverse shear  
failure mode



# POST-BUCKLING OF A COMPOSITE PANEL UNDER IN-PLANE LOADING

## Finite Element Models

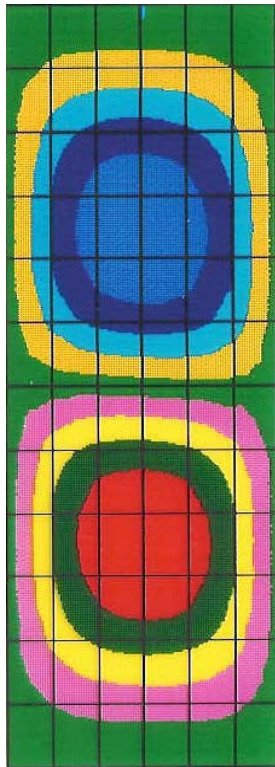
- Mesh has six elements per buckling mode half wave in each direction
- Elements used:
  - (1) Four-node  $C^1$  -based flat shell element (STAGS)
  - (2) Nine-node continuum shell element (Chao & Reddy)
  - (3) For-node and nine-node ANS shell elements (Park & Stanley)
- All meshes have 72 elements (91 nodes for the meshes with four-node elements and 325 nodes for meshes with nine-node elements).



# Comparison of the Experimental (Moire) and Analytical Out-of-Plane Deflection Patterns

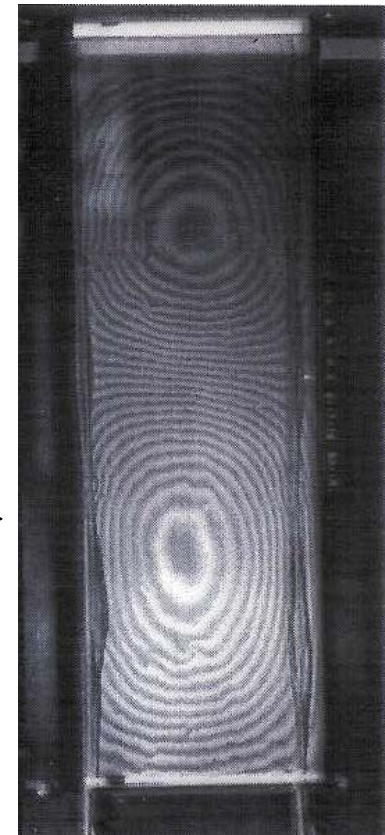
Theoretical (FEM)

Experimental

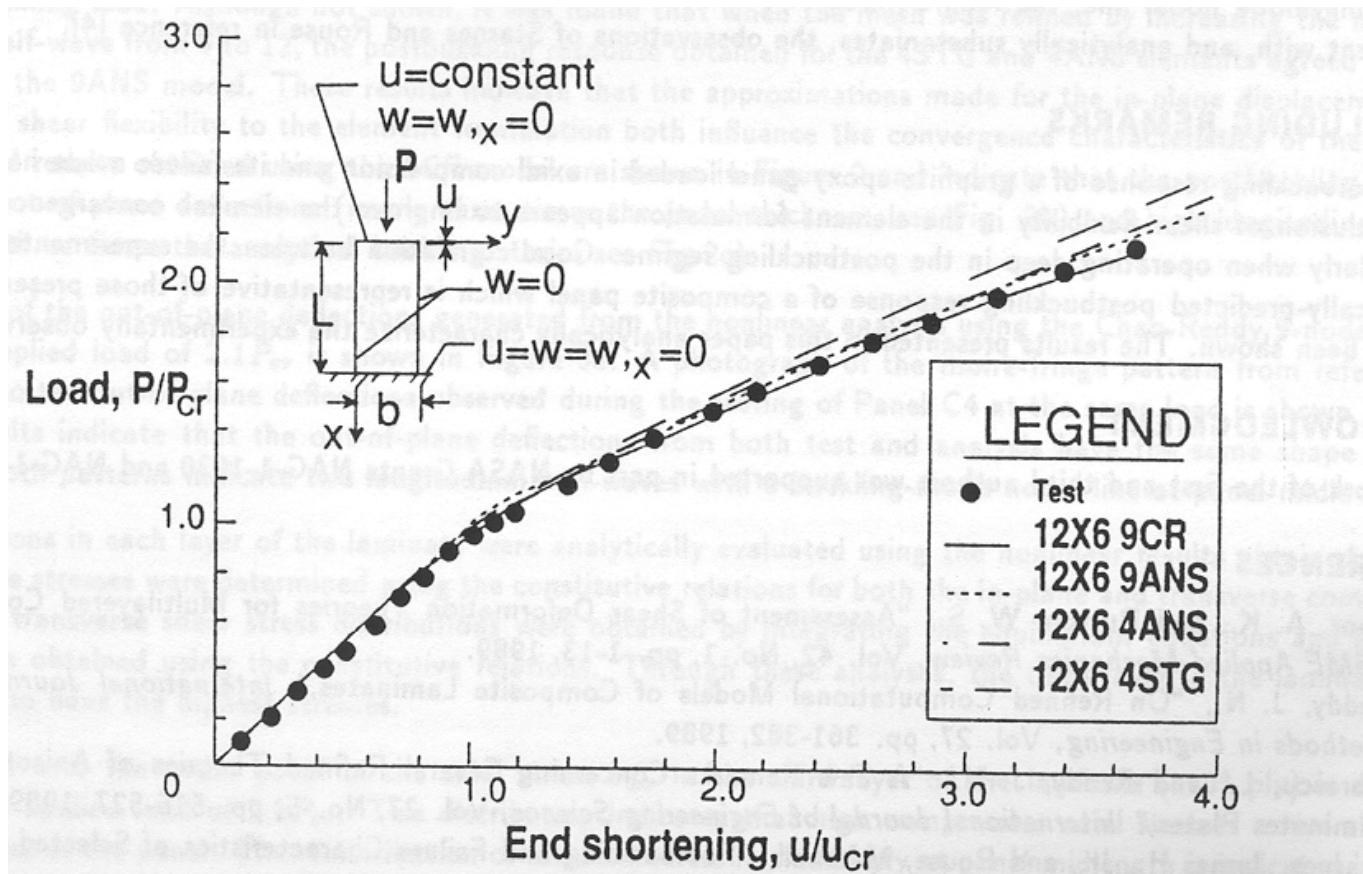


◀ (a) Contour plot of the analytical results

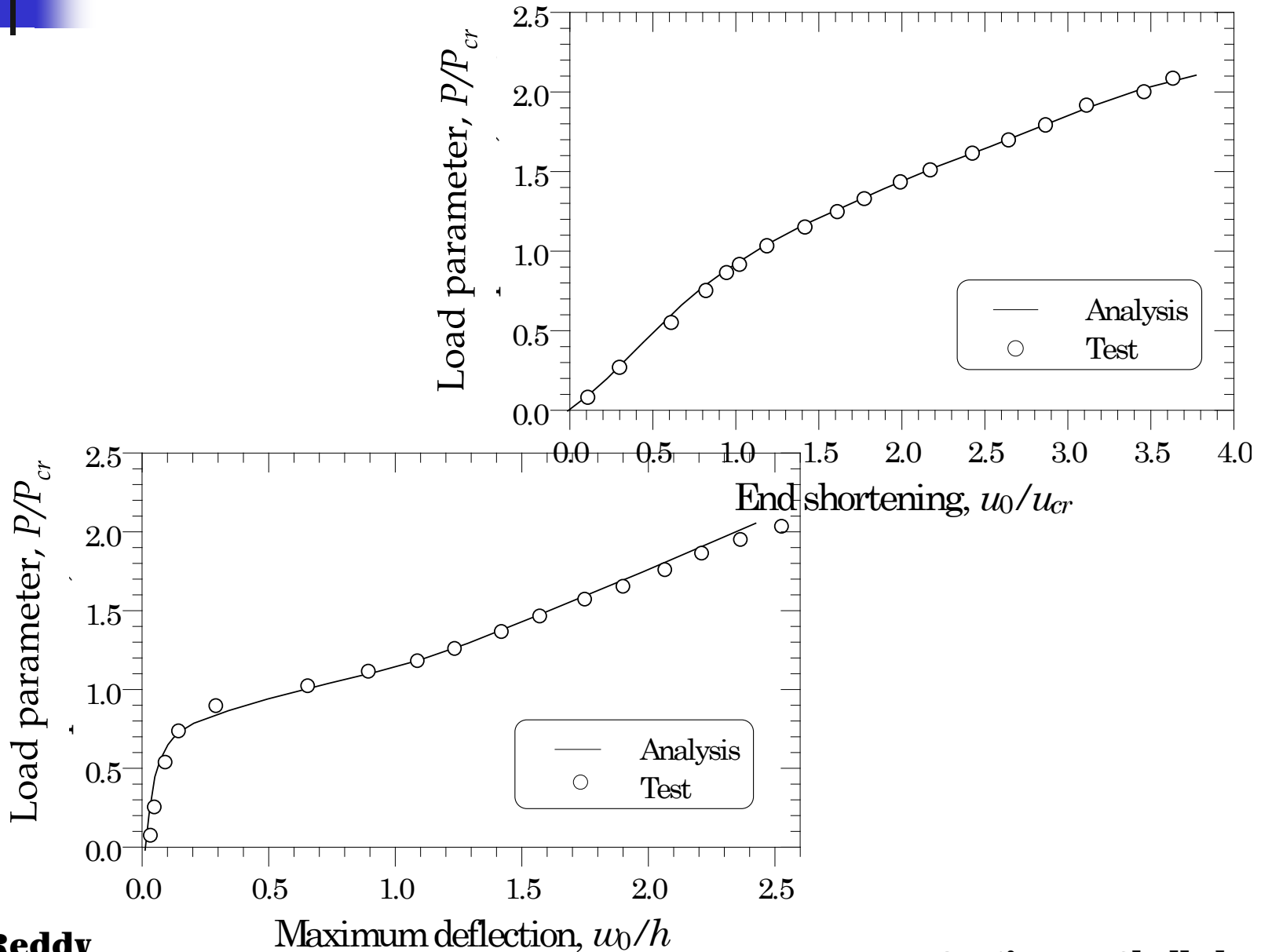
(b) Photograph of Moiré fringe pattern ▶



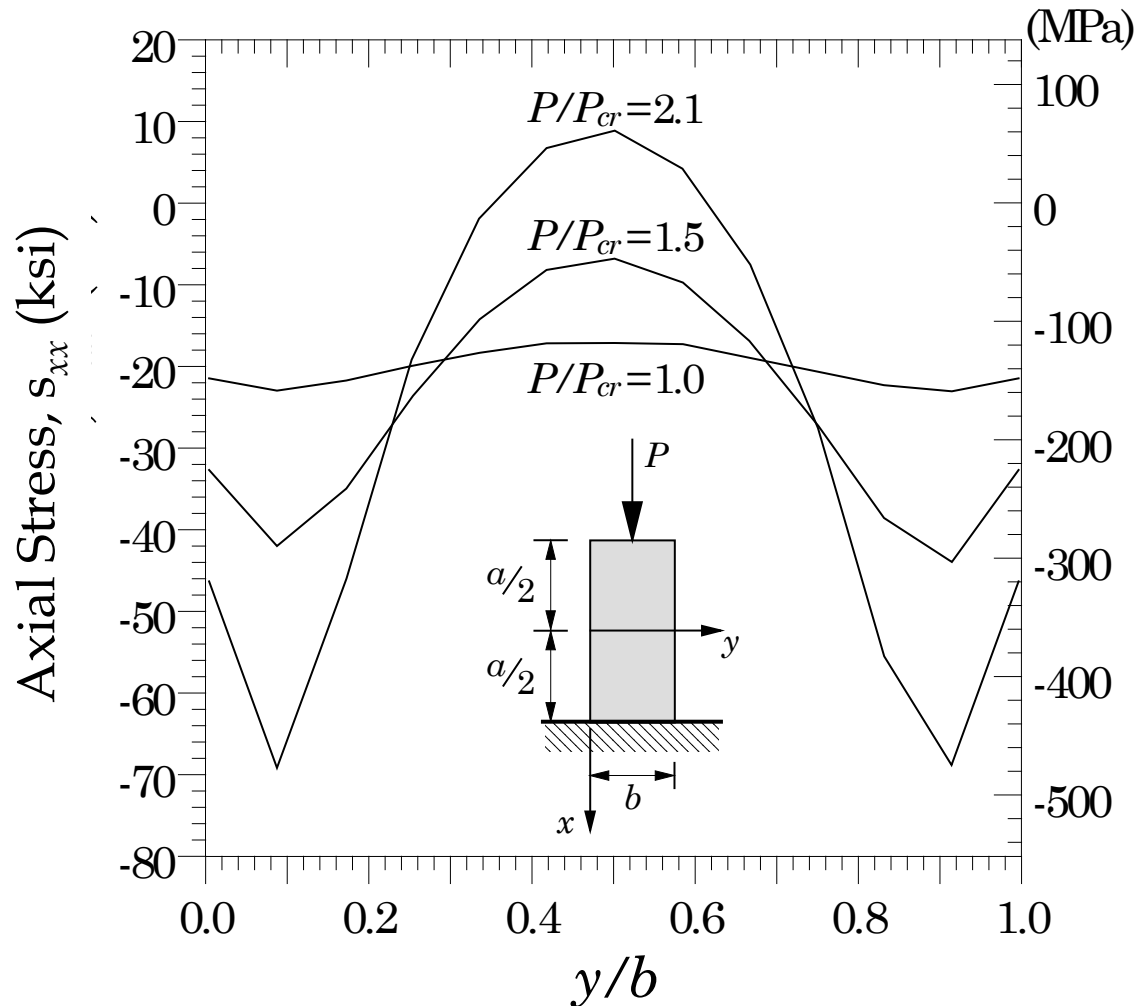
# Comparison of the Experimental and Analytical Solutions for End Shortening



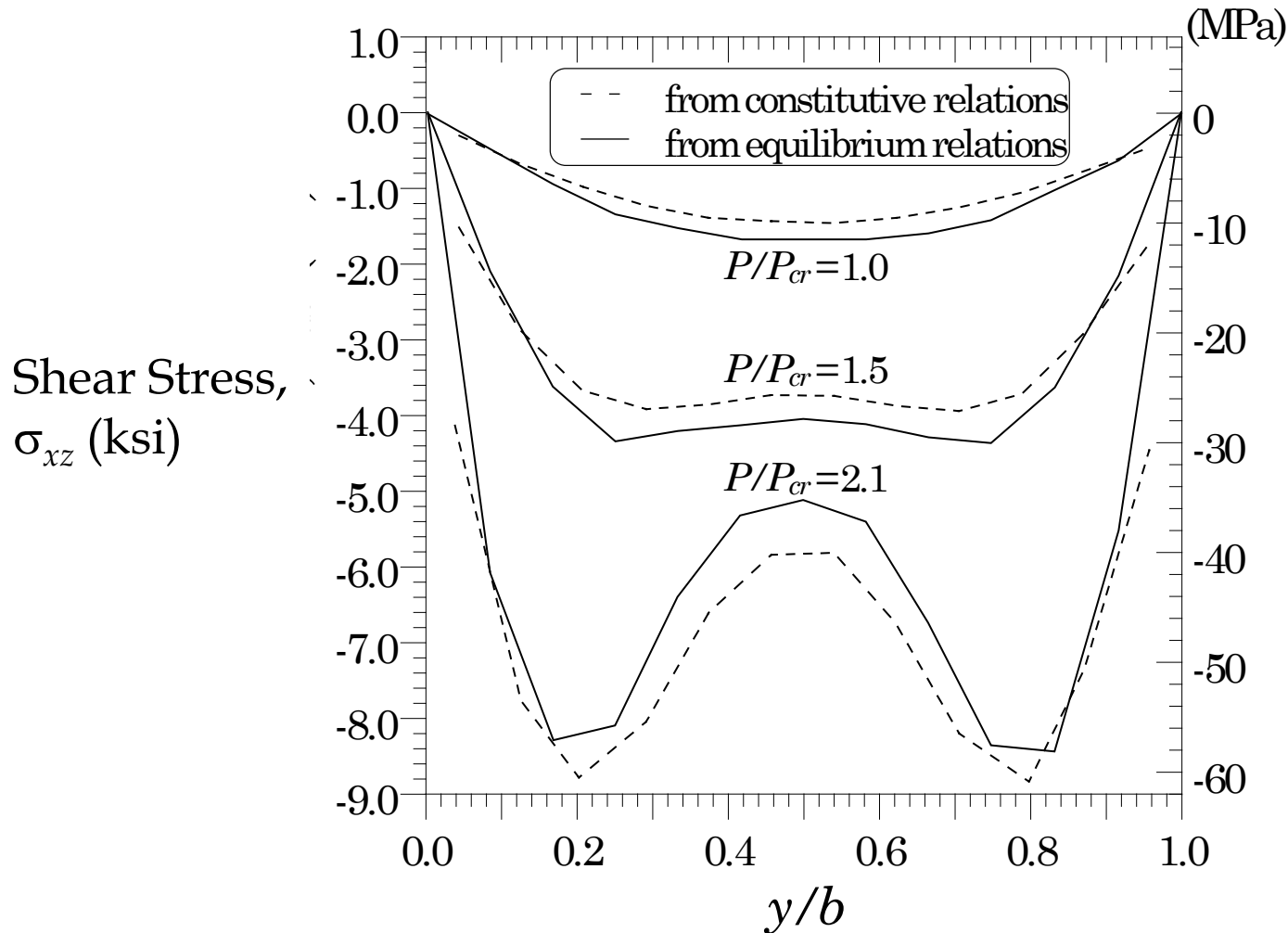
# Postbuckling of a Composite Panel



# Postbuckling of a Composite Panel (Stress Distributions)



# Postbuckling of a Composite Panel (Stress Distributions)





# SUMMARY

- **Description of continuum shell element (principle of virtual displacements conjugate pairs, decompositions, approximation of the geometry and displacement field)**
- **Post-buckling analysis of composite panels and comparison with experimental results (problem description, boundary conditions, fringe patterns of the displacement field, post-buckling path; failure analysis)**