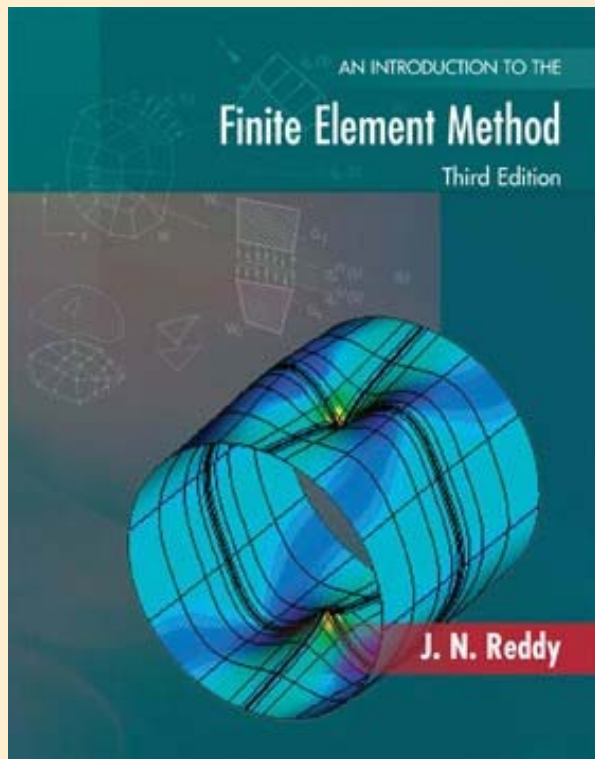


# The Finite Element Method

## 2D Flows of Viscous Incompressible Fluids

**Read: Chapter 10**



### CONTENTS

- **Governing Equations of Flows of Incompressible Fluids**
- **Mixed (Velocity-Pressure) Finite Element Model**
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- **Numerical Results**
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# Governing Equations of Flows of Viscous incompressible Fluids

## Equations of motion

$$\nabla \cdot \boldsymbol{\sigma} + \mathbf{f} = \rho \frac{D\mathbf{v}}{Dt} \Rightarrow$$

$$\frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \sigma_{xy}}{\partial y} + f_x = \rho \frac{Dv_x}{Dt}$$

$$\frac{\partial \sigma_{xy}}{\partial x} + \frac{\partial \sigma_{yy}}{\partial y} + f_y = \rho \frac{Dv_y}{Dt}$$

## Material time derivative

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla \Rightarrow \frac{D}{Dt} = \frac{\partial}{\partial t} + v_x \frac{\partial}{\partial x} + v_y \frac{\partial}{\partial y}$$

## Conservation of mass

$$\nabla \cdot \mathbf{v} = 0 \Rightarrow$$

$$\frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} = 0$$

## Constitutive relations

$$\boldsymbol{\sigma} = -P\mathbf{I} + \boldsymbol{\tau}, \quad \boldsymbol{\tau} = 2\mu\mathbf{D}$$

# Governing Equations of Flows of Viscous incompressible Fluids

## Kinematics relations

$$\mathbf{D} = \frac{1}{2} \left[ \nabla \mathbf{v} + (\nabla \mathbf{v})^T \right] \Rightarrow D_{xx} = \frac{\partial v_x}{\partial x}, D_{yy} = \frac{\partial v_y}{\partial y}, 2D_{xy} = \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x}$$

## Stress-velocity-pressure relations

$$\sigma_{xx} = 2\mu \frac{\partial v_x}{\partial x} - P, \sigma_{yy} = 2\mu \frac{\partial v_y}{\partial y} - P, \sigma_{xy} = \mu \left( \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} \right)$$

## Boundary conditions

$$(v_x, t_x) \text{ and } (v_y, t_y)$$

$$t_x = \sigma_{xx} n_x + \sigma_{xy} n_y, t_y = \sigma_{xy} n_x + \sigma_{yy} n_y$$

# Governing Equations in Terms of Velocities and Pressure

## Differential equations

$$\rho \frac{\partial v_x}{\partial t} - \frac{\partial}{\partial x} \left( \underbrace{2\mu \frac{\partial v_x}{\partial x} - P}_{\sigma_{xx}} \right) - \frac{\partial}{\partial y} \left( \underbrace{\mu \left( \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} \right)}_{\sigma_{xy}} \right) - f_x = 0 \quad (1)$$

$$\rho \frac{\partial v_y}{\partial t} - \frac{\partial}{\partial x} \left( \underbrace{\mu \left( \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} \right)}_{\sigma_{xy}} \right) - \frac{\partial}{\partial y} \left( \underbrace{2\mu \frac{\partial v_y}{\partial y} - P}_{\sigma_{yy}} \right) - f_y = 0 \quad (2)$$

$$\left( \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} \right) = 0 \quad (3)$$

## Boundary conditions

$$(v_x, t_x) \text{ and } (v_y, t_y)$$

## Finite Element Models: Some comments

There are two possible finite element models with velocities and possibly pressure as the nodal variables.

The most natural finite element model is that based on Eqs. (1)–(3), and it includes  $(v_x, v_y, P)$  as the nodal variables. It is known as the mixed model. It should be noted that  $P$  is neither a primary variable nor a secondary variable (although it is a part of  $(t_x, t_y)$ ). Often, pressure  $P$  presents numerical difficulties.

An alternative formulation that involves only  $(v_x, v_y)$  by treating Eq. (3) as a constraint. This is called the penalty finite element model.

# WEAK FORMS OF THE STOKES EQUATIONS

$$\begin{aligned}
 0 &= \int_{\Omega^e} w_1 \left[ \rho \frac{\partial v_x}{\partial t} - \frac{\partial}{\partial x} \left( 2\mu \frac{\partial v_x}{\partial x} - P \right) - \frac{\partial}{\partial y} \left( \mu \left( \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} \right) \right) - f_x \right] dx dy \\
 &= \int_{\Omega^e} \left[ \rho w_1 \frac{\partial v_x}{\partial t} - \frac{\partial w_1}{\partial x} \left( 2\mu \frac{\partial v_x}{\partial x} - P \right) - \mu \frac{\partial w_1}{\partial y} \left( \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} \right) - w_1 f_x \right] dx dy - \oint_{\Gamma^e} w_1 t_x ds \\
 0 &= \int_{\Omega^e} w_2 \left[ \rho \frac{\partial v_y}{\partial t} - \frac{\partial}{\partial y} \left( 2\mu \frac{\partial v_y}{\partial y} - P \right) - \frac{\partial}{\partial x} \left( \mu \left( \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} \right) \right) - f_y \right] dx dy \\
 &= \int_{\Omega^e} \left[ \rho w_2 \frac{\partial v_y}{\partial t} - \frac{\partial w_2}{\partial y} \left( 2\mu \frac{\partial v_y}{\partial y} - P \right) - \mu \frac{\partial w_2}{\partial x} \left( \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} \right) - w_2 f_y \right] dx dy - \oint_{\Gamma^e} w_2 t_y ds \\
 0 &= \int_{\Omega^e} w_3 \left( \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} \right) dx dy \quad \begin{aligned} &w_1 \approx v_x ; w_2 \approx v_y ; w_3 \approx -P \\ &t_x = \sigma_{xx} n_x + \sigma_{xy} n_y, \quad t_y = \sigma_{xy} n_x + \sigma_{yy} n_y \end{aligned}
 \end{aligned}$$

# Mixed Finite Element Model for the steady-static case

$$v_x = \sum_{j=1}^m v_{xj} \psi_j, \quad v_y = \sum_{j=1}^m v_{yj} \psi_j, \quad P = \sum_{j=1}^n P_j \phi_j$$

$$\begin{bmatrix} \mathbf{M}^{11} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{M}^{22} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} \end{bmatrix} \begin{Bmatrix} \dot{\mathbf{v}}_x \\ \dot{\mathbf{v}}_y \\ \dot{\mathbf{P}} \end{Bmatrix} + \begin{bmatrix} \mathbf{K}^{11} & \mathbf{K}^{12} & \mathbf{K}^{13} \\ \mathbf{K}^{21} & \mathbf{K}^{22} & \mathbf{K}^{23} \\ \mathbf{K}^{31} & \mathbf{K}^{32} & \mathbf{K}^{33} \end{bmatrix} \begin{Bmatrix} \mathbf{v}_x \\ \mathbf{v}_y \\ \mathbf{P} \end{Bmatrix} = \begin{Bmatrix} \mathbf{F}^1 \\ \mathbf{F}^2 \\ \mathbf{F}^3 \end{Bmatrix}$$

$$M_{ij}^{11} = M_{ij}^{22} = \int_{\Omega^e} \rho \psi_i \psi_j \, dx dy, \quad M_{ij}^{33} = M_{ij}^{12} = M_{ij}^{21} = M_{ij}^{31} = M_{ij}^{13} = M_{ij}^{23} = M_{ij}^{32} = 0$$

$$K_{ij}^{\alpha\beta} = K_{ji}^{\beta\alpha}, \quad K_{ij}^{11} = \int_{\Omega^e} \mu \left( 2 \frac{\partial \psi_i}{\partial x} \frac{\partial \psi_j}{\partial x} + \frac{\partial \psi_i}{\partial y} \frac{\partial \psi_j}{\partial y} \right) dx dy, \quad K_{ij}^{12} = \int_{\Omega^e} \mu \frac{\partial \psi_i}{\partial y} \frac{\partial \psi_j}{\partial x} dx dy$$

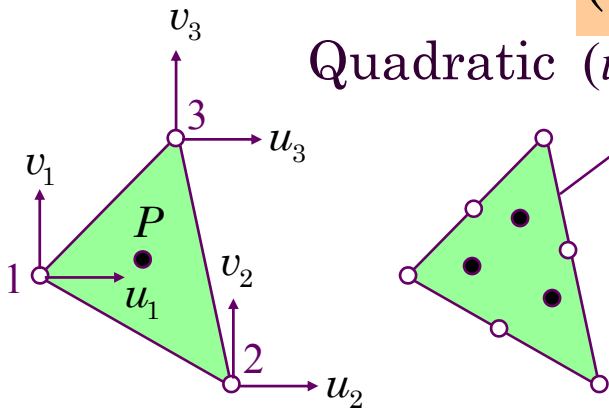
# Mixed Finite Element Model for the steady-static case (continued)

$$K_{ij}^{13} = \int_{\Omega^e} \mu \frac{\partial \psi_i}{\partial x} \phi_j \, dx dy, \quad K_{ij}^{23} = \int_{\Omega^e} \mu \frac{\partial \psi_i}{\partial y} \phi_j \, dx dy, \quad K_{ij}^{33} = 0$$

$$K_{ij}^{22} = \int_{\Omega^e} \mu \left( \frac{\partial \psi_i}{\partial x} \frac{\partial \psi_j}{\partial x} + 2 \frac{\partial \psi_i}{\partial y} \frac{\partial \psi_j}{\partial y} \right) dx dy, \quad K_{ij}^{21} = K_{ji}^{12}, \quad K_{ij}^{31} = K_{ji}^{13}, \quad K_{ij}^{32} = K_{ji}^{23}$$

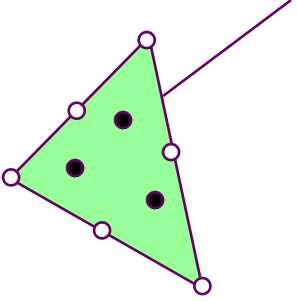
$$F_i^1 = \int_{\Omega^e} f_x \psi_i \, dx dy + \oint_{\Gamma^e} t_x \psi_i \, ds, \quad F_i^2 = \int_{\Omega^e} f_y \psi_i \, dx dy + \oint_{\Gamma^e} t_y \psi_i \, ds$$

$$(v_x, v_y) = (u, v)$$

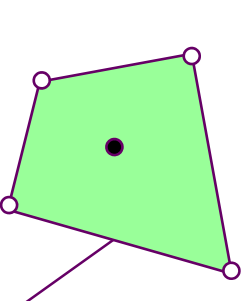


Linear  $(u, v)$ ; constant  $P$

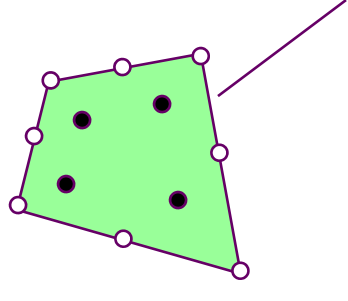
Quadratic  $(u, v)$ ; linear  $P$



Quadratic  $(u, v)$ ; linear  $P$



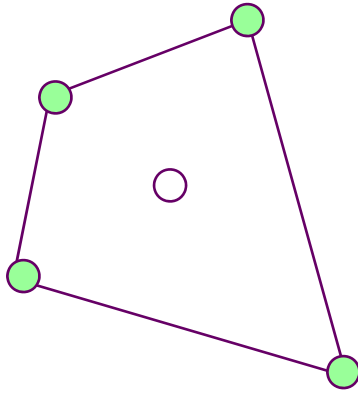
Linear  $(u, v)$ ; constant  $P$



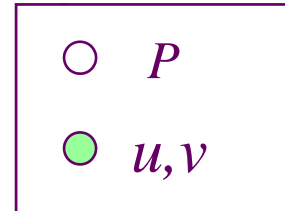


# 2D Elements Used for Viscous Incompressible Flows

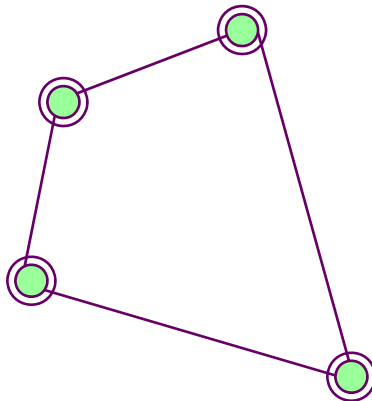
Q4C



Continuous bilinear displacements/velocities and discontinuous constant pressure (**checker board pattern is observed for pressure**)

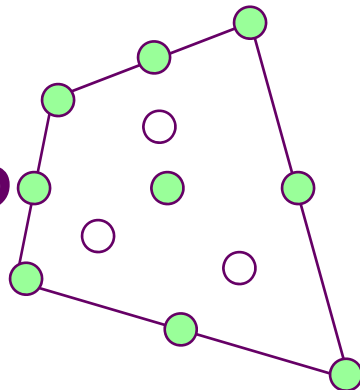


Q4



Continuous bilinear displacements/velocities and continuous bilinear pressure

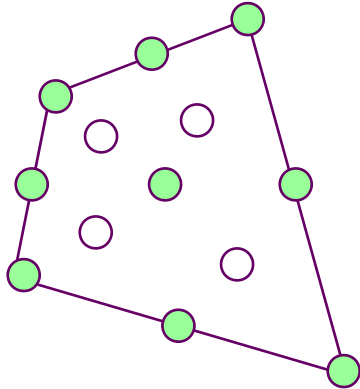
Q9L3-D



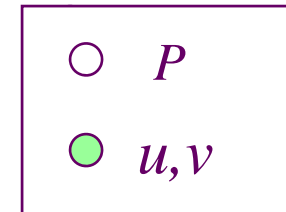
Continuous biquadratic displacements/velocities and discontinuous linear pressure (*works well*)

## 2D Elements Used for Viscous Incompressible Flows

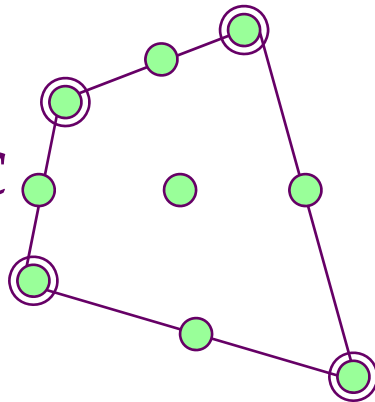
**Q9L4-D**



Continuous biquadratic displacements/velocities and discontinuous bilinear pressure



**Q9L4-C**



Continuous biquadratic displacements/velocities continuous linear pressure (*works well*)

# Penalty Function Method-*algebraic*

Problem: Find the minimum of the function  $F(x, y)$  subject to the constraint  $G(x, y) = 0$

$$dF \equiv \frac{\partial F}{\partial x} dx + \frac{\partial F}{\partial y} dy = 0$$

Lagrange multiplier method

$$F_L(x, y, \lambda) \equiv F(x, y) + \lambda G(x, y)$$

$$\begin{aligned} dF_L &\equiv \frac{\partial F_L}{\partial x} dx + \frac{\partial F_L}{\partial y} dy + \frac{\partial F_L}{\partial \lambda} d\lambda = 0 \\ &= \left( \frac{\partial F}{\partial x} + \lambda \frac{\partial G}{\partial x} \right) dx + \left( \frac{\partial F}{\partial y} + \lambda \frac{\partial G}{\partial y} \right) dy + G(x, y) d\lambda \end{aligned}$$

$$\frac{\partial F}{\partial x} + \lambda \frac{\partial G}{\partial x} = 0, \quad \frac{\partial F}{\partial y} + \lambda \frac{\partial G}{\partial y} = 0, \quad G(x, y) = 0$$

## Penalty Function Method-*algebraic* (continued)

Penalty function method

$$F_P(x, y) = F(x, y) + \frac{\gamma}{2}[G(x, y) - 0]^2$$

$$\begin{aligned} dF_P &\equiv \frac{\partial F_P}{\partial x} dx + \frac{\partial F_P}{\partial y} dy = 0 \\ &= \left( \frac{\partial F}{\partial x} + \gamma G(x, y) \frac{\partial G}{\partial x} \right) dx + \left( \frac{\partial F}{\partial y} + \gamma G(x, y) \frac{\partial G}{\partial y} \right) dy \end{aligned}$$

$$\frac{\partial F}{\partial x} + \gamma G(x, y) \frac{\partial G}{\partial x} = 0, \quad \frac{\partial F}{\partial y} + \gamma G(x, y) \frac{\partial G}{\partial y} = 0$$

$$\begin{aligned}
 dF_L &\equiv \frac{\partial F_L}{\partial x} dx + \frac{\partial F_L}{\partial y} dy + \frac{\partial F_L}{\partial \lambda} d\lambda = 0 \\
 &= \left( \frac{\partial F}{\partial x} + \lambda \frac{\partial G}{\partial x} \right) dx + \left( \frac{\partial F}{\partial y} + \lambda \frac{\partial G}{\partial y} \right) dy + G(x, y) d\lambda
 \end{aligned}$$

$$\frac{\partial F}{\partial x} + \lambda \frac{\partial G}{\partial x} = 0,$$

$$\frac{\partial F}{\partial y} + \lambda \frac{\partial G}{\partial y} = 0,$$

$$G(x, y) = 0$$

$$\begin{aligned}
 dF_P &\equiv \frac{\partial F_P}{\partial x} dx + \frac{\partial F_P}{\partial y} dy = 0 \\
 &= \left( \frac{\partial F}{\partial x} + \gamma G(x, y) \frac{\partial G}{\partial x} \right) dx + \left( \frac{\partial F}{\partial y} + \gamma G(x, y) \frac{\partial G}{\partial y} \right) dy
 \end{aligned}$$

$$\frac{\partial F}{\partial x} + \gamma G(x, y) \frac{\partial G}{\partial x} = 0,$$

$$\frac{\partial F}{\partial y} + \gamma G(x, y) \frac{\partial G}{\partial y} = 0$$

Approximation of the Lagrange multiplier can be computed in the penalty method from

$$\lambda_\gamma = \gamma G(x_\gamma, y_\gamma)$$

# Penalty Function Method-*algebraic*

## (An Example)

$$F(x, y) = 2x^2 + y^2 - 8x + y + 1, \quad G(x, y) \equiv 2x - y = 0$$

*Lagrange Multiplier Method*

$$4x - 8 + 2\lambda = 0, \quad 2y + 1 - \lambda = 0, \quad 2x - y = 0$$

$$x = 0.5, \quad y = 1.0, \quad \lambda = 3.0$$

*Penalty Function Method*

$$4x - 8 + 2\gamma(2x - y) = 0, \quad 2y + 1 - \gamma(2x - y) = 0$$

$$x_\gamma = \frac{8 + 3\gamma}{4 + 6\gamma}, \quad y_\gamma = \frac{3\gamma - 1}{2 + 3\gamma}$$

Clearly, as  $\gamma \rightarrow \infty$ , we have

$$\lim_{\gamma \rightarrow \infty} x_\gamma = 0.5 = x, \quad \lim_{\gamma \rightarrow \infty} y_\gamma = 1.0 = y$$

# Penalty Function Method-*algebraic*

(Example - continued)

Table: A comparison of the penalty solution with the exact for various values of the penalty parameter  $\gamma$ .

$\gamma$	1.0	10.0	25.0	50.0	100.0	1000.0
$x_\gamma$	1.1	0.5938	0.5390	0.5197	0.5099	0.5010
$y_\gamma$	0.4	0.9063	0.9610	0.9803	0.9901	0.9990
$G(x_\gamma, y_\gamma)$	1.8	0.2813	0.1169	0.0592	0.0298	0.0030
$\lambda_\gamma$	1.8	2.8125	2.9221	2.9605	2.9801	2.9980

$$\lambda_\gamma = \gamma G(x_\gamma, y_\gamma)$$

# Penalty Function Method – *continuum (Beam Example)*

*Original Problem:* Minimize the total potential energy

$$\begin{aligned} \Pi^e(w_0) = & \int_{x_a}^{x_b} \left[ \frac{D_{xx}}{2} \left( \frac{d^2 w_0}{dx^2} \right)^2 - qw_0 \right] dx - w_0(x_a) \bar{Q}_1^e - w_0(x_b) \bar{Q}_3^e \\ & - \left( -\frac{dw_0}{dx} \right)_{x_a} \bar{Q}_2^e - \left( -\frac{dw_0}{dx} \right)_{x_b} \bar{Q}_4^e \end{aligned}$$

*New Problem:* Minimize the total potential energy

$$\begin{aligned} \Pi^e(w_0, \varphi) = & \int_{x_a}^{x_b} \left[ \frac{D_{xx}}{2} \left( \frac{d\varphi}{dx} \right)^2 - qw_0 \right] dx - w_0(x_a) \bar{Q}_1^e - w_0(x_b) \bar{Q}_3^e \\ & + \varphi(x_a) \bar{Q}_2^e + \varphi(x_b) \bar{Q}_4^e \end{aligned}$$

subject to the constraint

$$G(w_0, \varphi) \equiv \frac{dw_0}{dx} - \varphi(x) = 0$$



# Penalty Function Method: *Beam Example - continued*

$$\begin{aligned}
 I_P^e(w_0, \varphi) &= \Pi^e(w_0, \varphi) + \frac{1}{2} \int_{x_a}^{x_b} \gamma(x) [G(w_0, \varphi)]^2 dx \\
 &= \int_{x_a}^{x_b} \left[ \frac{D_{xx}}{2} \left( \frac{d\varphi}{dx} \right)^2 - qw_0 \right] dx - w_0(x_a) \bar{Q}_1^e - w_0(x_b) \bar{Q}_3^e \\
 &\quad + \varphi(x_a) \bar{Q}_2^e + \varphi(x_b) \bar{Q}_4^e + \frac{1}{2} \int_{x_a}^{x_b} \gamma \left[ \frac{dw_0}{dx} - \varphi \right]^2 dx
 \end{aligned}$$

$$\begin{aligned}
 0 &= \int_{x_a}^{x_b} \left[ D_{xx} \frac{d\varphi}{dx} \frac{d\delta\varphi}{dx} + \gamma \left( \frac{dw_0}{dx} - \varphi \right) \left( \frac{d\delta w_0}{dx} - \delta\varphi \right) - q\delta w_0 \right] dx \\
 &\quad - \delta w_0(x_a) \bar{Q}_1^e - \delta w_0(x_b) \bar{Q}_3^e + \delta\varphi(x_a) \bar{Q}_2^e + \delta\varphi(x_b) \bar{Q}_4^e
 \end{aligned}$$

# Penalty Function Method: *Beam Example - continued*

$$w_0 = \sum_{j=1}^m w_j \psi_j^{(1)}, \quad \varphi = \sum_{j=1}^n s_j \psi_j^{(2)}$$

$$\begin{bmatrix} [K^{11}] & [K^{12}] \\ [K^{21}] & [K^{22}] \end{bmatrix} \begin{Bmatrix} \{w\} \\ \{s\} \end{Bmatrix} = \begin{Bmatrix} \{F^1\} \\ \{F^2\} \end{Bmatrix}$$

$$K_{ij}^{11} = \int_{x_a}^{x_b} \gamma \frac{d\psi_i^{(1)}}{dx} \frac{d\psi_j^{(1)}}{dx} dx, \quad K_{ij}^{12} = - \int_{x_a}^{x_b} \gamma \frac{d\psi_i^{(1)}}{dx} \frac{d\psi_j^{(2)}}{dx} dx = K_{ji}^{21}$$

$$K_{ij}^{22} = \int_{x_a}^{x_b} \left( D_{xx} \frac{d\psi_i^{(2)}}{dx} \frac{d\psi_j^{(2)}}{dx} + \gamma \psi_i^{(2)} \psi_j^{(2)} \right) dx$$

$$F_i^1 = \int_{x_a}^{x_b} q \psi_i^{(1)} dx + w_0(x_a) \bar{Q}_1^e + w_0(x_b) \bar{Q}_3^e$$

$$F_i^2 = -\varphi(x_a) \bar{Q}_2^e - \varphi(x_b) \bar{Q}_4^e$$

# PENALTY FORMULATION for flows of viscous incompressible fluids (for the Steady-State Case)

Consider the weak forms

$$0 = \int_{\Omega^e} \left[ \frac{\partial w_1}{\partial x} \left( 2\mu \frac{\partial v_x}{\partial x} - P \right) - \mu \frac{\partial w_1}{\partial y} \left( \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} \right) - w_1 f_x \right] dx dy$$

$$- \oint_{\Gamma^e} w_1 t_x ds$$

$$0 = \int_{\Omega^e} \left[ \mu \frac{\partial w_2}{\partial x} \left( \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} \right) + \frac{\partial w_2}{\partial y} \left( 2\mu \frac{\partial v_y}{\partial y} - P \right) - w_2 f_y \right] dx dy$$

$$- \oint_{\Gamma^e} w_2 t_y ds$$

$$0 = - \int_{\Omega^e} w_3 \left( \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} \right) dx dy, \quad \frac{\partial w_1}{\partial x} + \frac{\partial w_2}{\partial y} = 0$$

# Penalty Finite Element Formulation (continued)

Now suppose that the velocity field satisfies the constraint

$$\frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} = 0 \Rightarrow \frac{\partial w_1}{\partial x} + \frac{\partial w_2}{\partial y} = 0$$

Then adding the three weak statements, we obtain

$$0 = \int_{\Omega^e} \left[ 2\mu \frac{\partial w_1}{\partial x} \frac{\partial v_x}{\partial x} + 2\mu \frac{\partial w_2}{\partial y} \frac{\partial v_y}{\partial y} + \mu \left( \frac{\partial w_1}{\partial y} + \frac{\partial w_2}{\partial x} \right) \left( \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} \right) \right. \\ \left. - P \left( \frac{\partial w_1}{\partial x} + \frac{\partial w_2}{\partial y} \right) - w_3 \left( \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} \right) - w_1 f_x - w_2 f_y \right] dx dy \\ - \oint_{\Gamma^e} (w_1 t_x + w_2 t_y) ds$$

# Penalty Finite Element Formulation *- continued*

Thus, the weak form of the problem, subjected to the constraint is

$$0 = \int_{\Omega^e} \left[ 2\mu \frac{\partial w_1}{\partial x} \frac{\partial v_x}{\partial x} + 2\mu \frac{\partial w_2}{\partial y} \frac{\partial v_y}{\partial y} + \mu \left( \frac{\partial w_1}{\partial y} + \frac{\partial w_2}{\partial x} \right) \left( \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} \right) - w_1 f_x - w_2 f_y \right] dx dy - \oint_{\Gamma^e} (w_1 t_x + w_2 t_y) ds$$

Then, the modified weak form with the constraint is

$$0 = \int_{\Omega^e} \left[ 2\mu \frac{\partial w_1}{\partial x} \frac{\partial v_x}{\partial x} + 2\mu \frac{\partial w_2}{\partial y} \frac{\partial v_y}{\partial y} + \mu \left( \frac{\partial w_1}{\partial y} + \frac{\partial w_2}{\partial x} \right) \left( \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} \right) - w_1 f_x - w_2 f_y \right] dx dy - \oint_{\Gamma^e} (w_1 t_x + w_2 t_y) ds$$

$$+ \int_{\Omega^e} \gamma \left( \frac{\partial w_1}{\partial x} + \frac{\partial w_2}{\partial y} \right) \left( \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} \right) dx dy \leftarrow \text{Penalty expression}$$

## Penalty Finite Element Formulation - *continued*

The weak form of the problem can be separated into the following two statements

$$0 = \int_{\Omega^e} \left[ 2\mu \frac{\partial w_1}{\partial x} \frac{\partial v_x}{\partial x} + \mu \frac{\partial w_1}{\partial y} \left( \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} \right) + \gamma \frac{\partial w_1}{\partial x} \left( \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} \right) - w_1 f_x \right] dx dy$$

$$- \oint_{\Gamma^e} w_1 t_x ds$$

$$0 = \int_{\Omega^e} \left[ 2\mu \frac{\partial w_2}{\partial y} \frac{\partial v_y}{\partial y} + \mu \frac{\partial w_2}{\partial x} \left( \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} \right) + \gamma \frac{\partial w_2}{\partial y} \left( \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} \right) - w_2 f_y \right] dx dy$$

$$- \oint_{\Gamma^e} w_2 t_y ds$$

These statements form the basis of the penalty finite element model.

# Penalty Finite Element Formulation

(continued)

Alternatively, the pressure (negative of the Lagrange multiplier) in the governing equations can be replaced by

$$P_\gamma = -\gamma \left( \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} \right)$$

we obtain

$$\begin{aligned} -\frac{\partial}{\partial x} \left( 2\mu \frac{\partial v_x}{\partial x} \right) - \frac{\partial}{\partial y} \left[ \mu \left( \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} \right) \right] - \frac{\partial}{\partial x} \left[ \gamma \left( \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} \right) \right] - f_x &= 0 \\ -\frac{\partial}{\partial x} \left[ \mu \left( \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} \right) \right] - \frac{\partial}{\partial y} \left( 2\mu \frac{\partial v_y}{\partial y} \right) - \frac{\partial}{\partial y} \left[ \gamma \left( \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} \right) \right] - f_y &= 0 \end{aligned}$$

The weak forms of these equations are precisely the same as those on the previous slide.

# Penalty Finite Element Model

$$u_x = \sum_{j=1}^m u_{xj} \psi_j(x, y), \quad u_y = \sum_{j=1}^m u_{yj} \psi_j(x, y)$$

Substitution into the weak forms (adding inertia terms) yields the equations

$$\begin{bmatrix} \mathbf{M}^{11} & \mathbf{0} \\ \mathbf{0} & \mathbf{M}^{22} \end{bmatrix} \begin{Bmatrix} \dot{\mathbf{v}}_x \\ \dot{\mathbf{v}}_y \end{Bmatrix} + \begin{bmatrix} \mathbf{K}^{11} & \mathbf{K}^{12} \\ \mathbf{K}^{21} & \mathbf{K}^{22} \end{bmatrix} \begin{Bmatrix} \mathbf{v}_x \\ \mathbf{v}_y \end{Bmatrix} = \begin{Bmatrix} \mathbf{F}^1 \\ \mathbf{F}^2 \end{Bmatrix}$$

$$M_{ij}^{11} = M_{ij}^{22} = \int_{\Omega^e} \rho \psi_i \psi_j \, dx dy$$

$$K_{ij}^{11} = \int_{\Omega^e} \mu \left( 2 \frac{\partial \psi_i}{\partial x} \frac{\partial \psi_j}{\partial x} + \frac{\partial \psi_i}{\partial y} \frac{\partial \psi_j}{\partial y} \right) dx dy + \int_{\Omega^e} \gamma \frac{\partial \psi_i}{\partial x} \frac{\partial \psi_j}{\partial x} dx dy$$

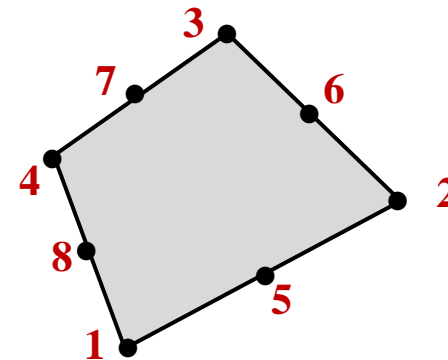
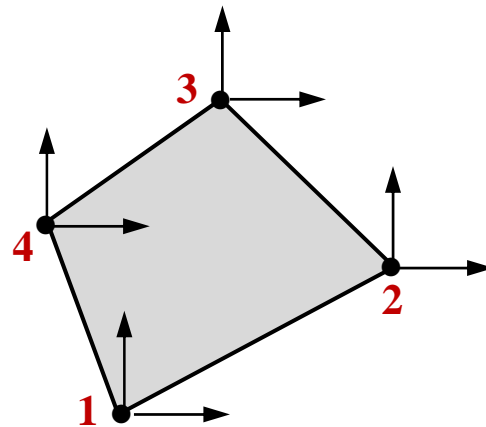
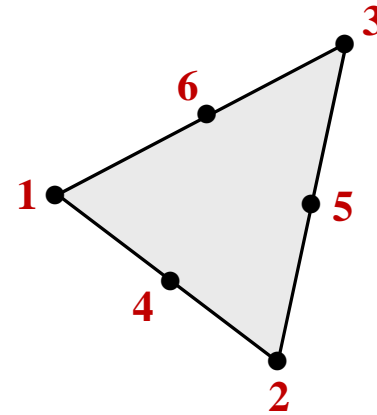
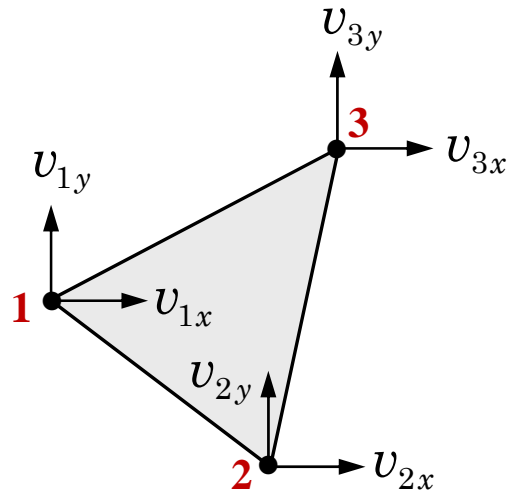
$$K_{ij}^{12} = \int_{\Omega^e} \mu \frac{\partial \psi_i}{\partial y} \frac{\partial \psi_j}{\partial x} dx dy + \int_{\Omega^e} \gamma \frac{\partial \psi_i}{\partial x} \frac{\partial \psi_j}{\partial y} dx dy, \quad K_{ij}^{21} = K_{ji}^{12}$$

$$K_{ij}^{22} = \int_{\Omega^e} \mu \left( \frac{\partial \psi_i}{\partial x} \frac{\partial \psi_j}{\partial x} + 2 \frac{\partial \psi_i}{\partial y} \frac{\partial \psi_j}{\partial y} \right) dx dy + \int_{\Omega^e} \gamma \frac{\partial \psi_i}{\partial y} \frac{\partial \psi_j}{\partial y} dx dy$$

$$F_i^1 = \int_{\Omega^e} f_x \psi_i \, dx dy + \oint_{\Gamma^e} t_x \psi_i \, ds, \quad F_i^2 = \int_{\Omega^e} f_y \psi_i \, dx dy + \oint_{\Gamma^e} t_y \psi_i \, ds$$



## Elements Used for Penalty FE Model



# Computational Aspects of the Penalty FEM

*General form of the Penalty FEM:*

$$(\mu[K^1] + \rho[K^2] + \gamma[K^3]) \{\Delta\} = \{F\}$$

*Element 'locking':*

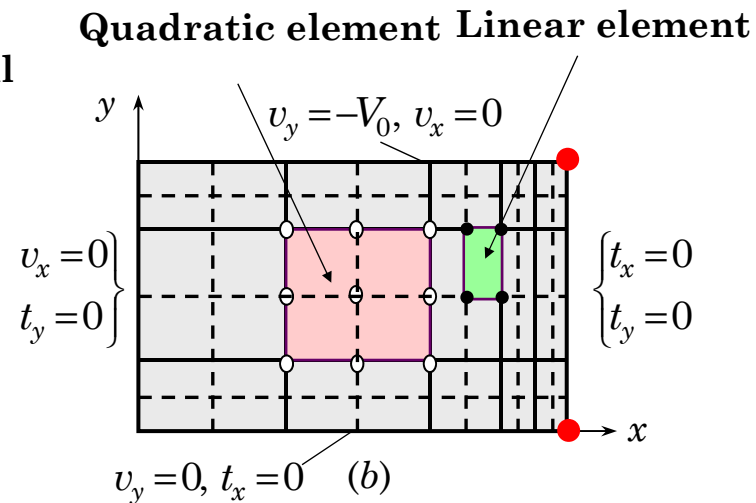
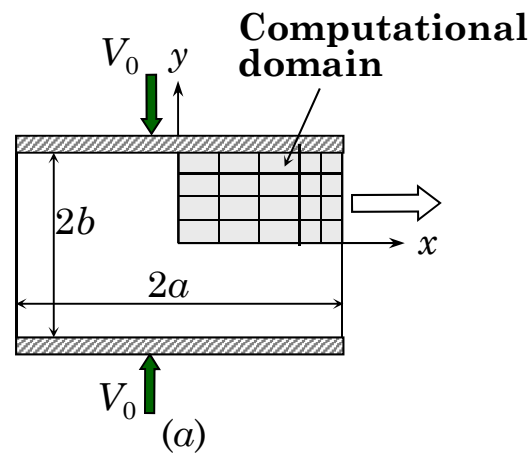
$$\lim_{\gamma \rightarrow 0} (\mu[K^1] + \rho[K^2] + \gamma[K^3]) \{\Delta\} = \{F\} \rightarrow \gamma[K^3]\{\Delta\} = \{F\}$$

*Choice of the penalty parameter:*

$$\gamma = 10^4 \mu \text{ to } \gamma = 10^{12} \mu$$

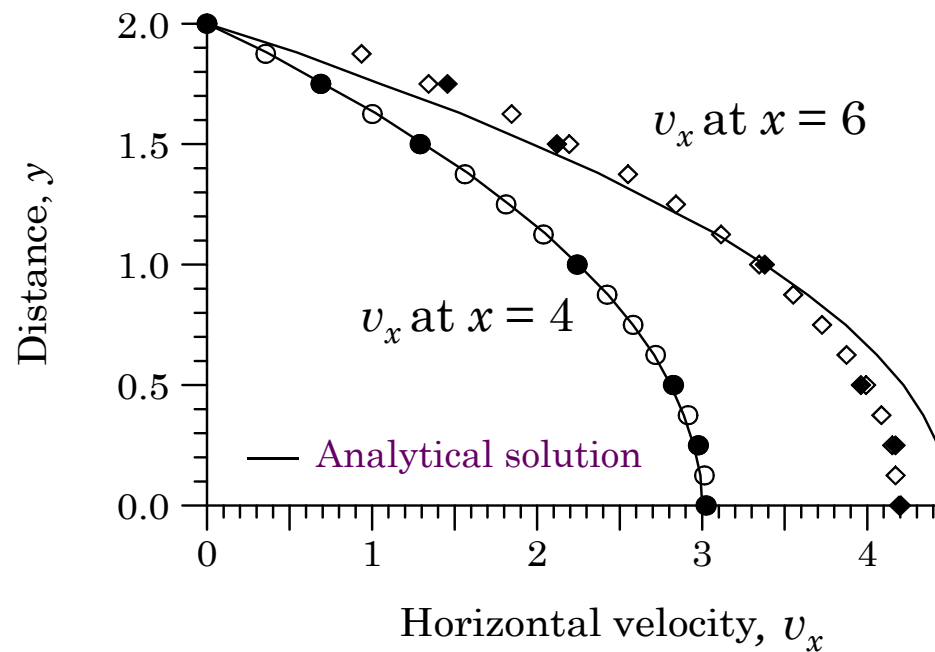
# Numerical Examples

## Viscous fluid squeezed between parallel plates

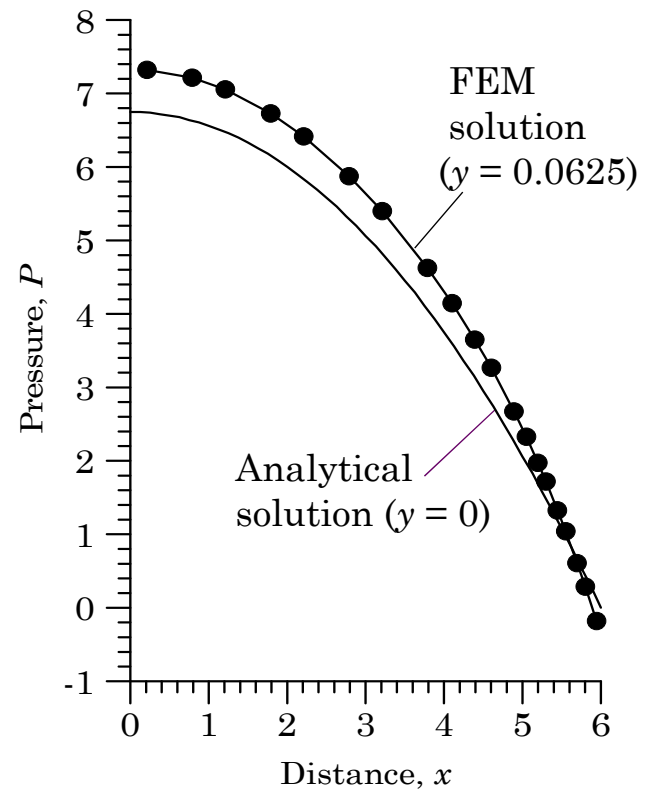
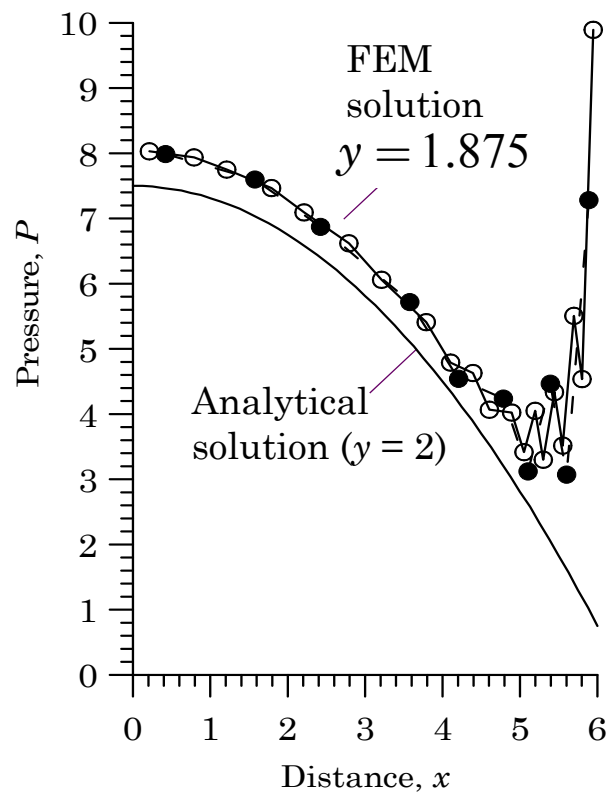


- **Note:** There are singularities in the application of the boundary conditions

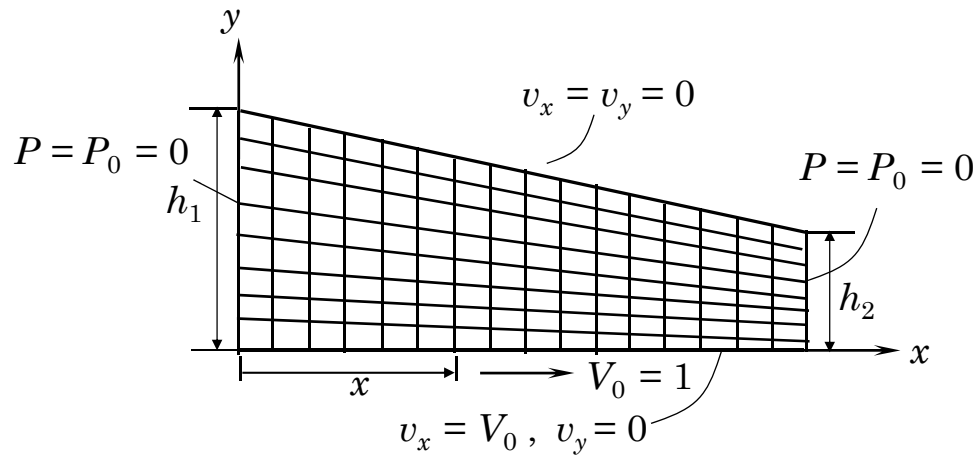
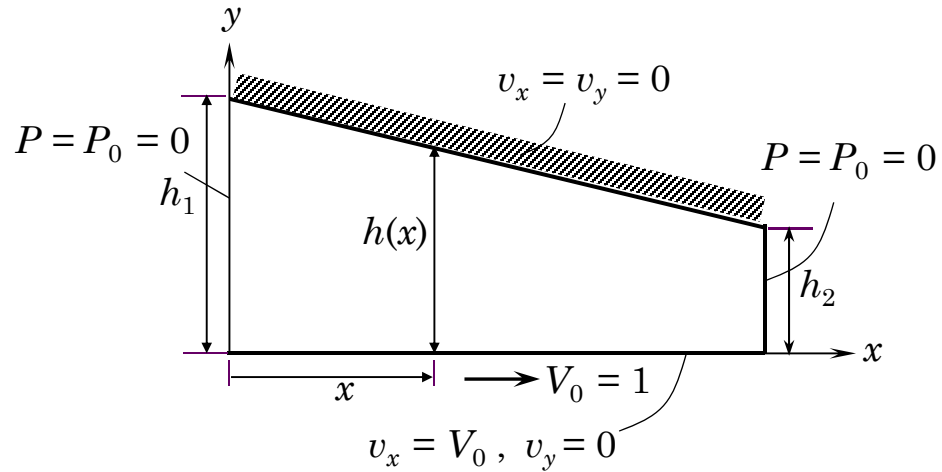
# Viscous fluid squeezed between parallel plates: Velocity field



# Viscous fluid squeezed between parallel plates: Pressure field

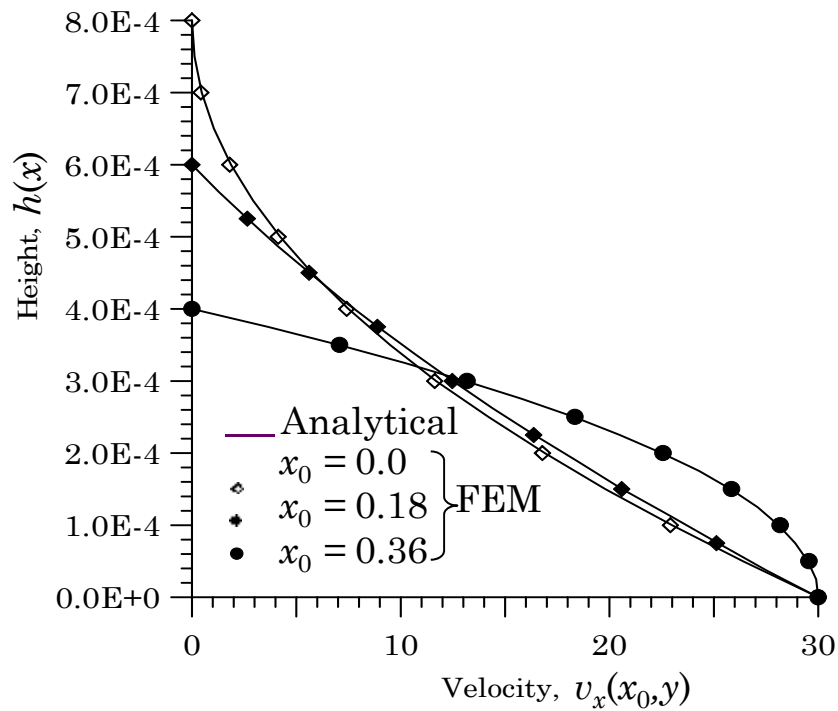


## 2. Flow of a viscous lubricant in a slider bearing

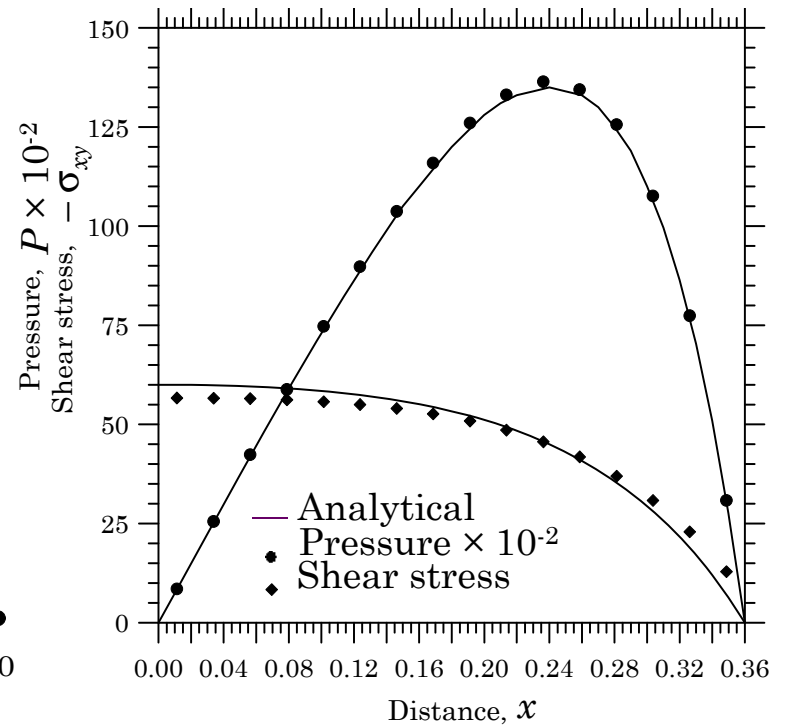


# Flow of a viscous lubricant in a slider bearing

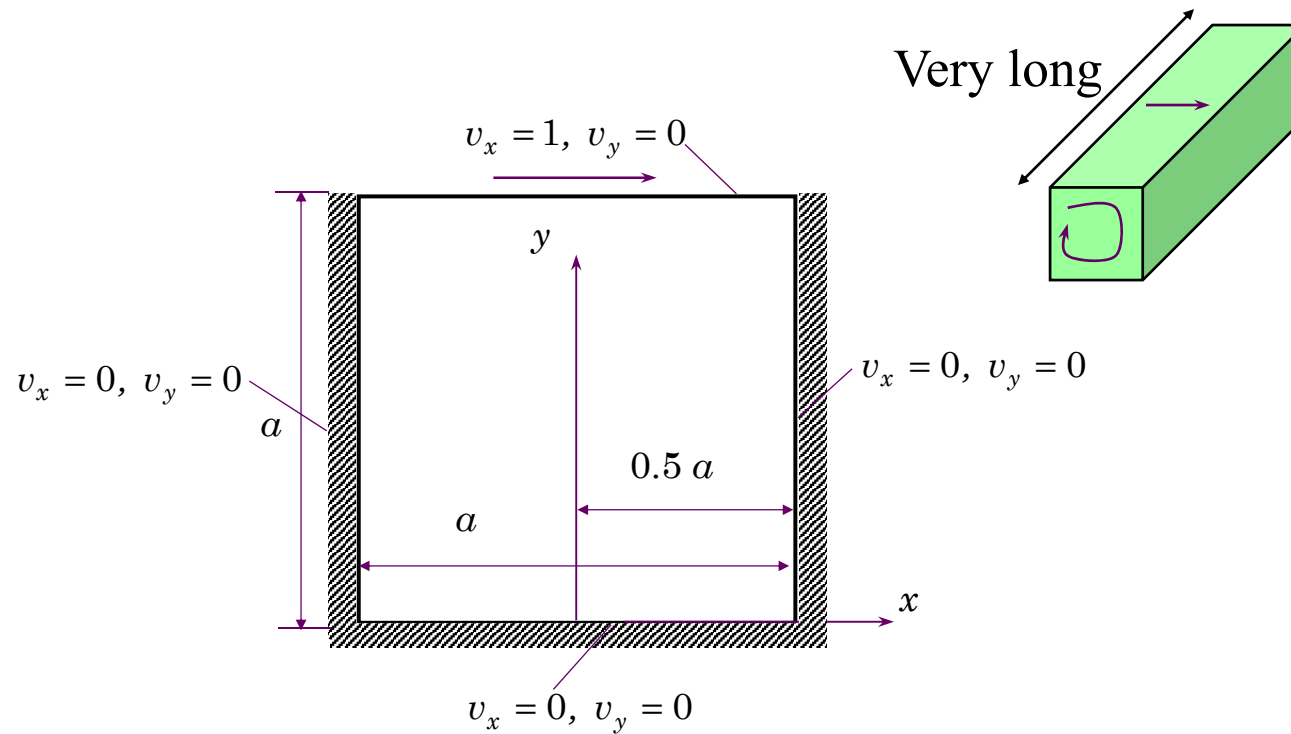
## Velocity field



## Pressure field

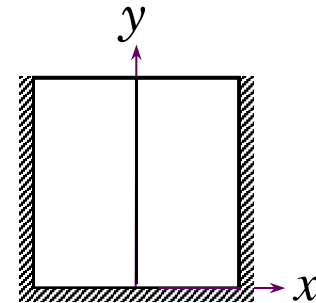
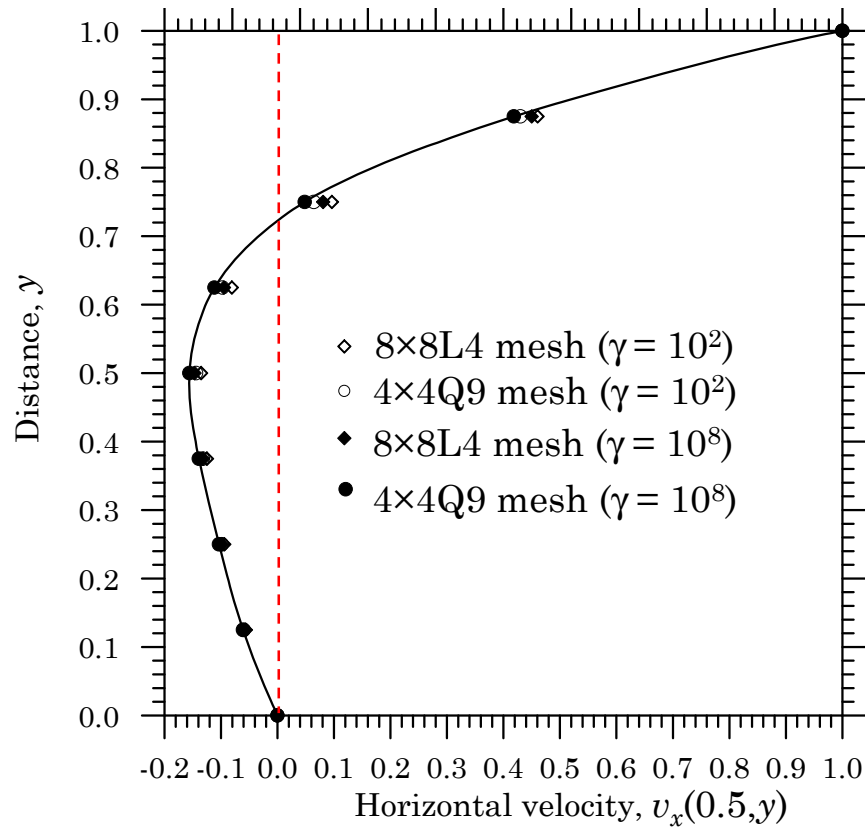


### 3. Wall-driven cavity flow

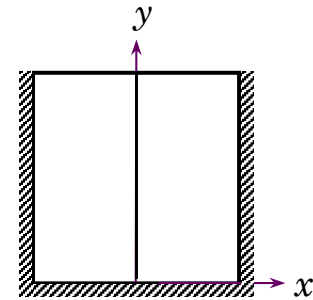
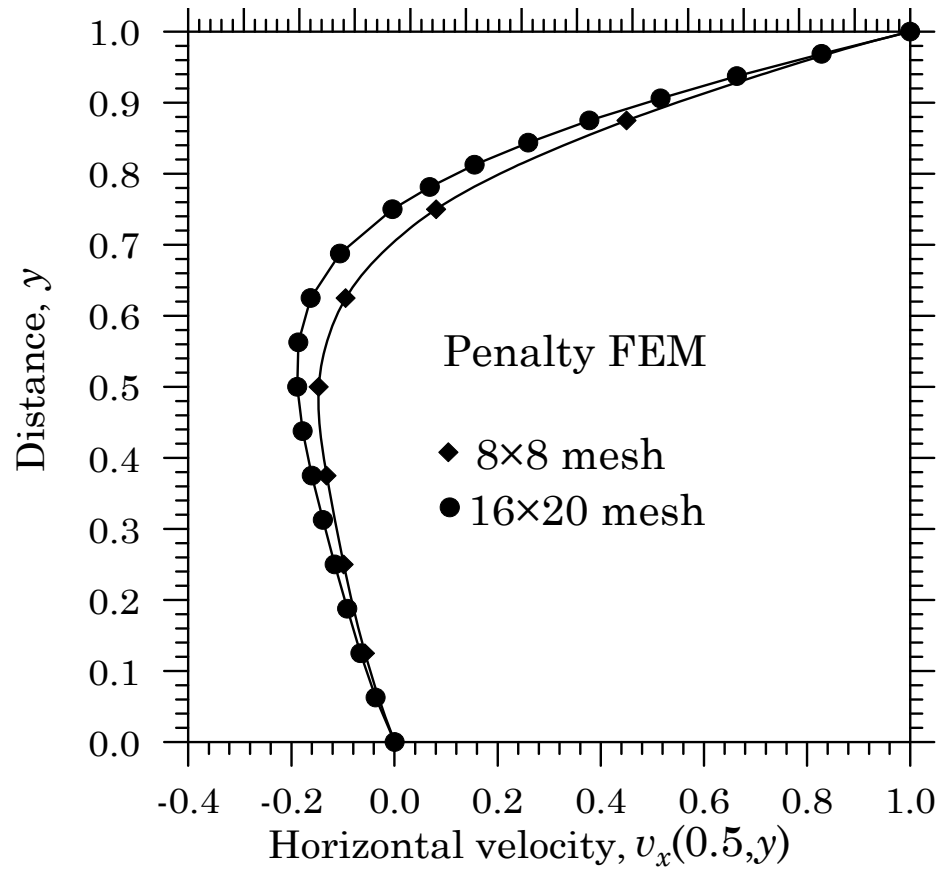




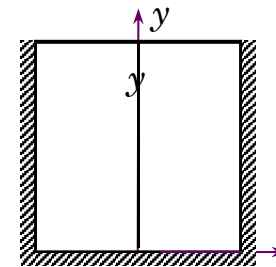
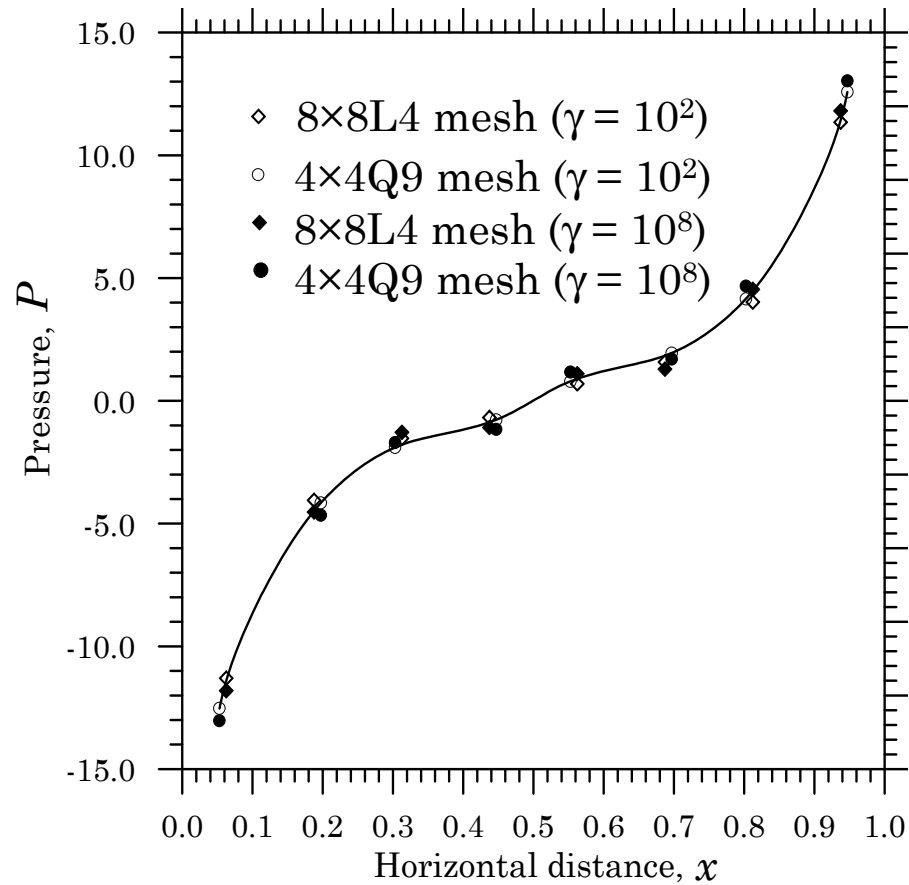
# Wall-driven cavity flow – velocity profiles



# Wall-driven cavity flow – velocity profiles



# Wall-driven cavity flow – Pressure profile



# SUMMARY

**The following topics were covered:**

- **Governing equations of flows of incompressible fluids**
- **Mixed (velocity-pressure) finite element model**
- **Penalty function method - *algebraic problem***
- **Penalty finite element model of viscous incompressible fluids**
- **Numerical results**